

**THEORY & OBJECTIVE**

# **ELECTRICAL MACHINES**

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**CORPORATE OFFICE**

100-102, Ram Nagar, Bambala Puliya, Tonk Road, Pratap Nagar, Jaipur-302033

**Ph.: + 91-8094441777**

**Website : [www.engineersacademy.org](http://www.engineersacademy.org) | Email: [info@engineersacademy.org](mailto:info@engineersacademy.org)**

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## TRANSFORMERS

### THEORY

#### 1.1 COMPARISON BETWEEN MAGNETIC AND ELECTRIC CIRCUITS

Parameters	Magnetic Circuit	Electric Circuit
Circuit		
1. Definition	The closed path followed by magnetic flux is called a magnetic circuit	The closed path followed by an electric current is called an electric circuit.
2. Driving force	MMF is required to establish flux $\phi$ in the magnetic circuit and is measured in ampere-turns (AT) or amperes.	EMF is required to cause flow of current in an electric circuit and is measured in volts.
3. Response	$\text{Flux, } \phi = \frac{\text{Driving force}}{\text{Magnetic reluctance}}$ $= \frac{AT}{S} \text{ webers}$	$\text{Current, } I = \frac{\text{Driving force}}{\text{Electric resistance}}$ $= \frac{E}{R} \text{ ampere}$
4. Impedance	$\text{Reluctance, } S = \frac{l}{\mu_0 \mu_r a} = \frac{l}{\mu a} \text{ AT/Wb}$	$\text{Resistance, } R = \rho \frac{l}{a} \text{ ohms}$
(a) For series circuits	$S = S_1 + S_2 + S_3 + \dots$	$R = R_1 + R_2 + R_3 + \dots$
(b) For parallel circuits	$S = \frac{1}{\frac{1}{S_1} + \frac{1}{S_2} + \frac{1}{S_3} + \dots}$	$R = \frac{1}{\frac{1}{R_1} + \frac{1}{R_2} + \frac{1}{R_3} + \dots}$

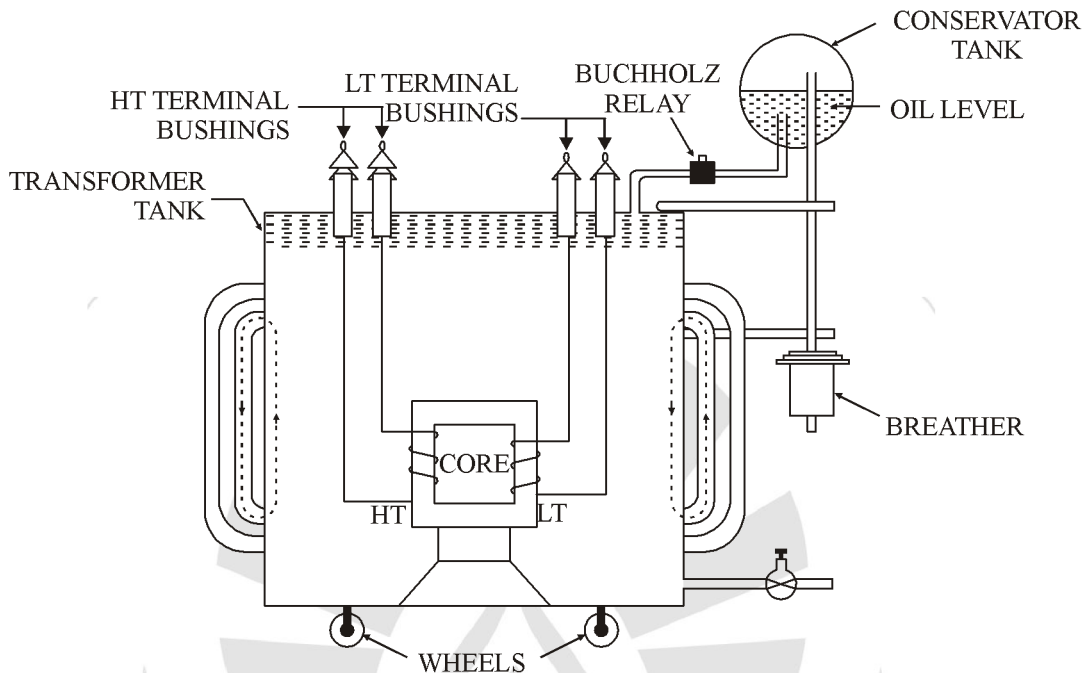
5. Admittance	Permeance = $\frac{1}{\text{Reluctance}}$ in Wb/AT	Conductance = $\frac{1}{\text{Resistance}}$ in siemens
6. Proportionality constant	Reluctivity = $\frac{1}{\text{Permeability}} = \frac{1}{\mu}$ in m/H	Resistivity, $\rho = \frac{1}{\text{Conductivity}}$ in $\Omega\text{-m}$
7. Density	Flux density,  $B = \mu \times \text{magnetic field intensity}$  $= \mu H$ tesla or $\text{Wb/m}^2$	Current density,  $J = \frac{\text{Electric field intensity}}{\rho}$ in $\text{A/m}^2$
8. Field intensity	Magnetic field intensity,  $H = \frac{\text{MMF}}{\ell} = \frac{NI}{\ell}$ in AT/m	Electric field intensity  $= \frac{E}{\ell}$ in volts/meter
9. Drop	MMF drop = $\phi \times \text{reluctance} = \phi S$	Voltage drop = $I \times \text{Resistance} = IR$

### DISSIMILARITIES

1. Flux does not actually flow in a magnetic circuit.	Current does flow in an electric circuit.
2. Permeability does not largely vary from material to material and there is hardly any material which can act as an insulator to the magnetic flux.	Conductivity varies largely from material to material so much so that some materials are insulators to electric current and some are very good conductors.
3. For a particular temperature the permeability depends up on the flux density (or total flux).	For a particular temperature, conductivity (or resistivity) is constant and independent of current strength.
4. Flux can pass through air.	Current would not flow through the air until an arc is struck.
5. Residual flux persists after removal of mmf.	The current is reduced to zero after removal of source of emf.
6. There is no waste of energy due to reluctance in the magnetic circuit and, therefore, energy is required only to create the magnetic flux but not to maintain it.	In an electric circuit, resistance causes heat to be generated resulting in waste of energy and, therefore, energy is required as long as the current flows.

## 1.2 TRANSFORMER CONSTRUCTION

The transformer is very simple in construction and consists of magnetic circuit linking with two windings known as primary and secondary windings.



- 1. Core Construction:** A transformer core is the steel system which forms the magnetic circuit with all parts pertaining to its construction. Those parts of the magnetic circuit, which carry the transformer windings are called the limbs or legs, and those parts which connect the legs and serve for closing the magnetic circuit are termed yokes.

The use of steel in magnetic circuit introduces iron or core loss but ensures a high permeability of the magnetic circuit. Because of high permeability the magnitude of exciting current necessary to create the required flux in the core, is small. The magnetic frame (cores and yokes) of the transformer is built up of laminated electrotechnic steel. The transformer grade steel consisting of 3.5% silicon.

The steel used for transformer cores may be hot rolled or cold rolled. The hot rolled steel which permitted a maximum flux density of 1.45 T was in use for a considerable length of time. In recent years this type of steel has been completely superseded by cold rolled steel allowing much higher flux densities up to 1.8 T to be used because it has better magnetic properties in the direction of rolling. Although, cold rolled steel is 25-35% more expensive than the hot rolled steel and needs special methods of core assembly. As the flux in the cores is pulsating one, it becomes necessary that the transformer cores are laminated and the laminations should be insulated and made as thin as practicable in order to reduce the eddy current loss or a minimum.

The thickness of laminations or stamping varies from 0.35mm to 0.5mm. The thickness should not be made below 3.0mm because in that case, the laminations becomes mechanically weak and tend to buckle. As a rule, the cores of high-capacity power transformers (for more than 100 kVA) are assembled of 0.5mm steel sheets, since such a construction is less labour consuming than with 0.35mm sheets. The laminations are insulated from each other by a very thin coating of varnish or by using 0.03mm thick paper. Paper insulation is much cheaper than varnish, but its heat resisting and heat-conducting properties and mechanical strength are worse. Besides, paper insulation occupies too large a percentage of the stack cross section. For this reason in high capacity power transformers, where these drawbacks are significant, varnish insulation is used.

**2. Windings :** Transformer windings are made of solid or stranded Copper or Aluminium strip conductors. Heavy current capacity needs conductors of large cross section. To reduce eddy current losses in the conductors, several small wires or parallel straps are preferred to one large strap.

On small transformers rectangular concentric coils are practical, but in a large unit the high repulsion forces generated between the primary and secondary coils under short-circuit conditions tend to "round out" the flat sides of the outer coil, if this happens, the resulting damage to the coil insulation will usually make the transformer unserviceable. Cylindrical concentric coils are the obvious answer to this problem of mechanical strength.

According to their arrangement high and low voltage windings can be either concentric (i.e., the windings, which in each cross section are circles with a common centre or sandwich, in which parts of the hv and lv windings alternate along the height of the leg. Concentric windings are employed in core type transformers as shown in fig (b). Whereas sandwiched windings are almost exclusively used in shell type transformers as shown in fig (f). On account of the easier insulation facilities, the low-voltage windings is placed nearer to the core in the case of concentric windings and on the outside positions in the case of sandwiched windings. The insulation spaces between low and high-voltage coils also serve to facilitate cooling.

The concentric windings used for core types of transformers can further be classified in many groups, the most important are (i) cylindrical windings, (ii) helical winding, (iii) crossover windings and (iv) continuous disc winding. (v) sandwich windings

**(i) Cylindrical Windings :** These windings are layered type and use either rectangular (or strip) or round conductors. If the cross section of a turn does not exceed 8 to 10 mm<sup>2</sup>, the cylindrical winding is made multi-layer of round conductor for a larger turn cross section the winding is made of rectangular (or strip) conductor, usually double layer. Cylindrical windings with strip conductors is shown in Fig (a). The winding is made up of turns helically wound round the cylinder generatrix with the turns close to each other.

The cylindrical windings using circular conductors are mainly employed for hv windings with voltages 6.6, 11 or 33 kV for ratings up to 600–1000 kVA whereas those using round conductors are mainly employed for low-voltage windings up to 6.6 kV for ratings up to 600-750 kVA.

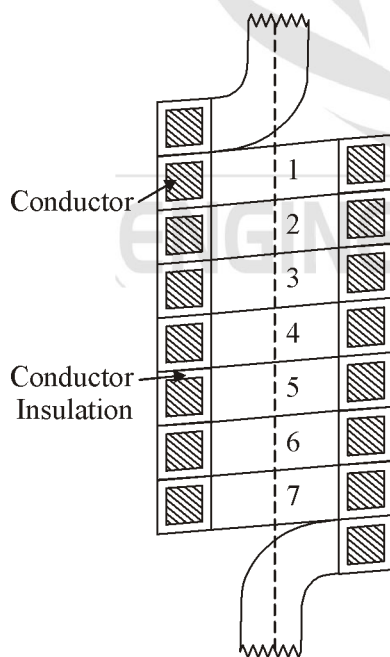


Fig. (a)

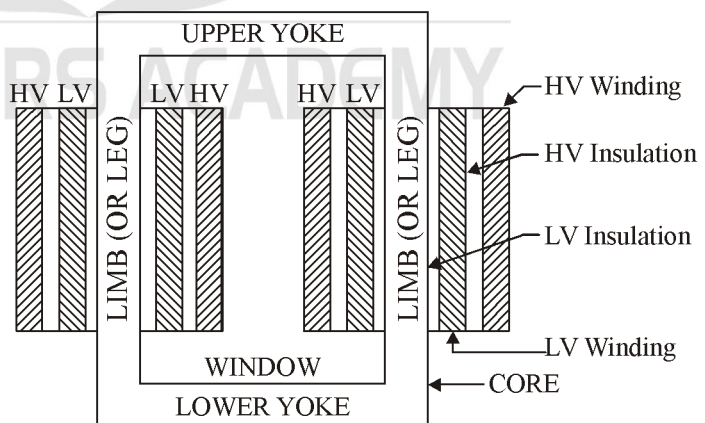


Fig. (b)

**(ii) Helical Windings :** Such windings are employed for lv coils of medium and high capacity transformers where the number of coil turns is small but the current is high (as high as 2,000 A).

Basically the helical winding is the same as the cylindrical windings except that in such windings between adjacent turns axial spacers are provided for duct formation to improve oil circulation for better cooling. The ducts are formed by spacers placed all the way round the periphery of the cylinder at regular intervals as shown in fig. (c).

Helical windings are employed in power transformers of rating ranging from 150 kVA to 30 MVA at voltages from 400V to 11kV and sometimes up to 33kV.

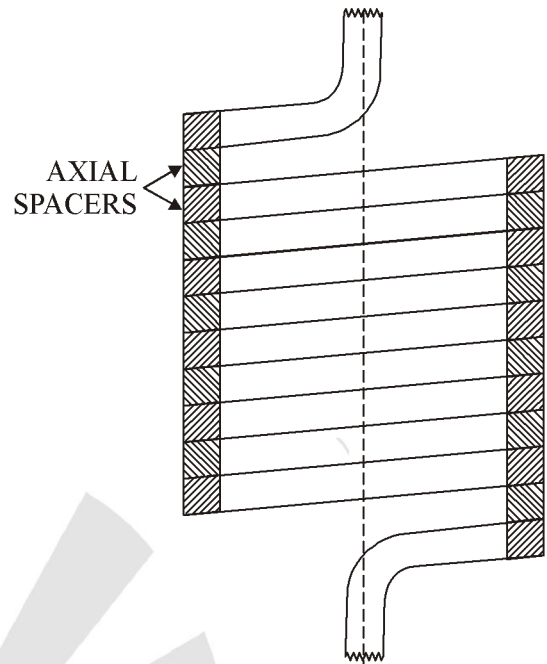
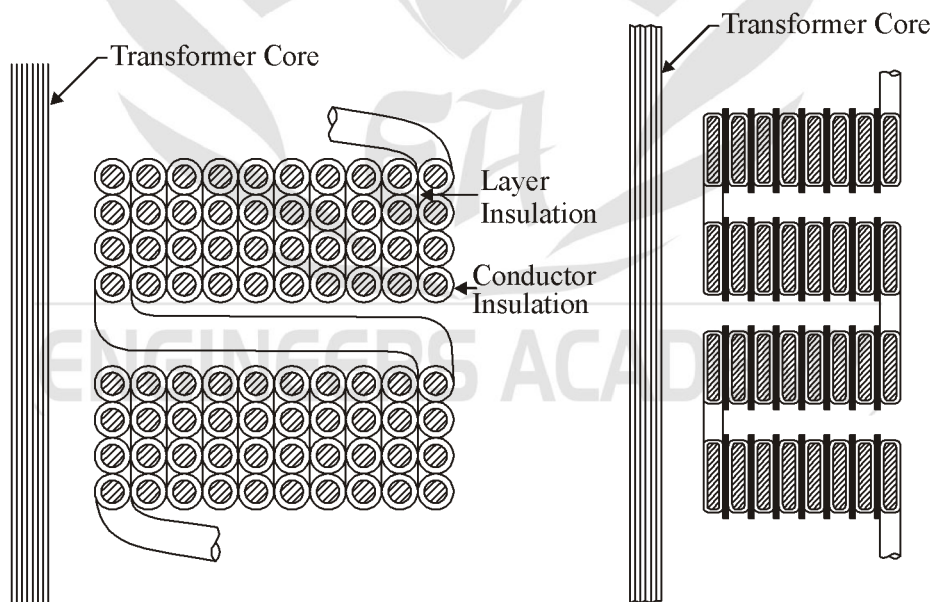


Fig. (c)

**(iii) Cross-over Windings :** Such windings are suitable for currents not exceeding 20A and are very largely employed for hv windings of low rating transformers where number of turns may be large but conductors are of small circular section with double cotton covering or paper covering.

The coil ends, one from inside and one from outside, are joined to other similar coils in series, spaced with blocks of insulating material to allow free circulation of oil.



(d) Cross-over Winding

(e) Continuous Disc Winding

**(iv) Continuous Disc Windings :** The disc coils, as their name suggests, consist of a number of flat coils or discs connected in series or parallel. The coils are formed with rectangular strips wound spirally from centre outwards in the radial direction, as illustrated in Fig. (e).

Continuous disc windings are reliable and strong and, therefore, they are widely employed both as lv and hv windings in large rating transformers.

- (v) **Sandwich Windings** : Such windings, as already mentioned, are most commonly employed in shell type transformers and allow easy control over leakage reactance. Leakage reactance can be reduced by subdividing the low and high voltage windings into a large number of sections or coils and arranging alternatively the hv and lv sections with the lv section nearer to the yoke, as illustrated in fig (f).

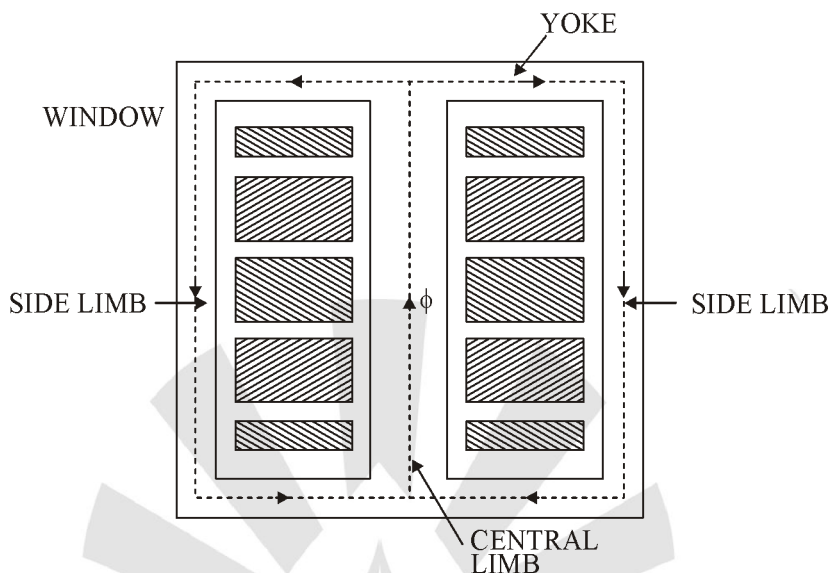


Fig. (f)

In comparison to concentric windings they have several drawbacks such as they are more labour consuming in manufacture, less stable in respect to short circuits and are more difficult to insulate from each other and from the yoke. This is the reason why the core type transformers with concentric windings are more common.

3. **Insulation** : Insulation used in a transformer may be classified into two parts major insulation and minor insulation. The insulation provided between windings and earthed parts (insulation provided between lv winding and core and between hv winding and yoke) and the insulation between the windings (insulation between primary and secondary windings) fall into the category of major insulation. In the interleaved construction the major insulation between windings usually consists of sheets of pressboard and oil ducts. Minor insulation includes the insulation provided between the elements of a given winding such as conductor insulation, insulation between turns, layers and coils. The minor insulation between the coils of the same winding usually consists of pressboard sheets and oil ducts. For very small units treated cloth or fibre may be used.

4. **Insulating Oil** : The insulating oil has three functions. It provides additional insulation, protects the insulation from dirt and moisture and it carries away the heat generated in the cores and coils.

It is obtained by fractional distillation of crude petroleum. Vegetable and animal oils are not used in transformers as they form fatty acids that attack the fibrous insulating materials used.

(i) High dielectric strength

(ii) Low viscosity to provide good heat transfer

(iii) **Purity** : The oil must not contain impurities such as acid, alkali and sulphur or its compounds to prevent corrosion of metal parts and insulation. Sulphur compounds, if present accelerate the formation of sludge.

(iv) **High flash point** : The temperature at which oil vapour ignites spontaneously is called the flash point. The flash point of transformer oil should not be less than 135°C.

(v) Free from sludging under normal operating conditions. Sludging means slow formation of semi-solid hydrocarbon owing to heating and oxidation. The sludge deposits itself on windings, tank walls and in cooling ducts. Sludges, being bad conductor of heat, greatly reduce the heat transfer from the windings to the oil and so increases the temperature of windings. Sometimes for preventing sludging certain chemicals called the inhibitors are added to the transformer oil.

(vi) Good resistance to emulsion so that the oil may throw down and moisture entering the apparatus instead of holding it in suspension.

5. **Tank** : Small capacity tanks are fabricated from welded sheet steel, while larger ones are assembled from plain boiler plates or cast-aluminium parts, usually mounted on a shallow fabricated steel base.

6. **Conservator or Expansion Tank** : The oil expands with the increase in load and contracts when the load decreases. Large power transformers are also liable to overloads which may overheat the oil and consequently there is a sludge formation if air is present.

This causes vapourisation of a part of the oil. The oil vapours form explosive mixture with air that ignites and may cause a considerable damage. For these reasons it is necessary to prevent the oil from having contact with air as well as moisture. For this purpose conservators are employed.

When the oil expands, the air is expelled out and air is drawn inside under contraction of oil. This process is termed breathing. Thus the oil is in contact with air.

Conservator is a small auxiliary oil tank (an airtight cylindrical metal drum) that may be mounted above the transformer and connected to the main tank by a pipe. Its function is to keep the main tank of the transformer completely filled with oil in all circumstances despite expansion or contraction of oil with the changes in temperature, conservator is always partly filled with oil and absorbs the expansion and contraction of oil and keeps the main tank full of oil. It also reduces the rate of oxidation of oil, partly because less oil surface is exposed to air and partly because of the reduced temperature of the oil exposed to air. Thus the sludge formation is considerably reduced and whatever sludge is formed settles to the bottom of the expansion chamber into a sludge pan from where it is periodically withdrawn by means of a drain tap. Normally the capacity of conservator should be approximately 10-12% of the oil volume of the main tank.

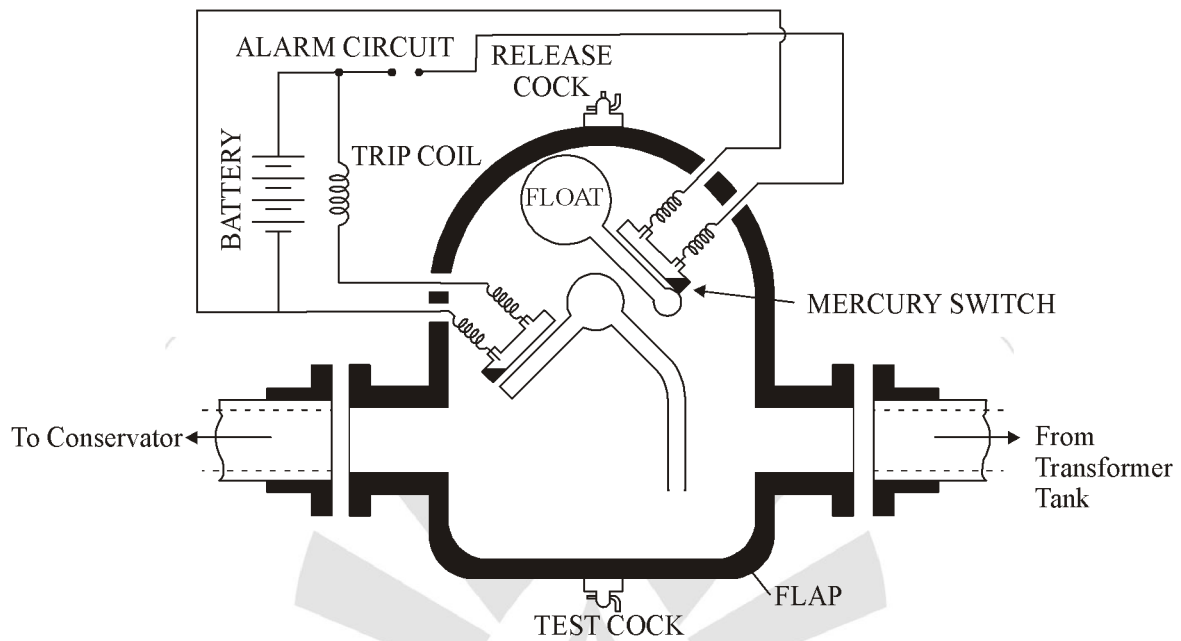
The expansion tank is usually installed on the low-voltage side of the transformer tank above the level of the transformer cover on a supporting frame.

7. **Breather** : When the transformer becomes warm, the oil and gas expand. The gas at the top of the oil is expelled out. When the transformer cools, air is drawn into the transformer. Unless preventive measures are taken, moisture is drawn during this process, called the breathing. This moisture is readily absorbed by the oil, and the dielectric properties of the oil are correspondingly reduced. The air entering the transformer is made moisture free by letting it pass through an apparatus called the breather. A breather consists of a small container connected to the vent pipe and contains a dehydrating material like silica gel crystals impregnated with cobalt chloride. The material is blue when dry and a whitish pink when damp. The colour can be observed through a glass window provided in front of container.

8. **Gas operated Relay - Buchholz Relay** : It is a gas and oil actuated protective device and it is practically universally used on all oil-immersed transformers having rating more than 500 kVA. It is installed in the pipe joining the main tank of the transformer to the conservator and is used to give alarm in case of minor fault and to disconnect the transformer from supply mains in case of severe internal fault. The use of such a relay is possible only with transformers having conservators.

When minor faults occur, heat is produced due to current leakage, some of the oil in the transformer tank evaporates and some vapour collects in the top of the chamber while passing to the conservator.

When a predetermined amount of vapour accumulates in the top of the chamber, the oil level falls, the mercury type switch attached to the float is tilted and closes the alarm circuit to ring the bell.



*Fig. Gas operated relay*

9. **Leads and Terminals :** The connections to the windings are by copper rods or bars, insulated wholly or in part, and taken to the bus-bars directly in the case of air cooled transformer, or to the insulator bushings mounted on the top of the transformer tank in case of oil cooled transformers.
10. **Bushings :** The bushing consists of a current carrying element in the form of a conducting rod, and a porcelain cylinder installed in the hole of the cover of the transformer and employed to isolate the current carrying element. Up to 33kV, ordinary porcelain insulators can be used. Above this voltage oil-filled or condenser type bushings are used.
11. **Tappings :** The transformers are usually provided with few tappings so that output voltage can be varied over a small range for constant input voltage. Most industrial transformers are provided with four tappings on the hv winding.

**Transformer :**

A Transformer is a static device comprising coupled coils (Primary and Secondary) wound on common magnetic Core.

MMF (F)

$$F = NI \text{ Amp. turns}$$

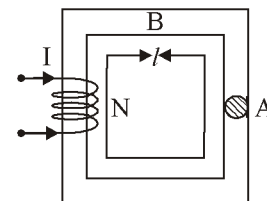
Let the mean core length =  $l$

$$\text{Flux density} = B, \text{ Flux } \phi = BA$$

A = Area of cross-section of core.

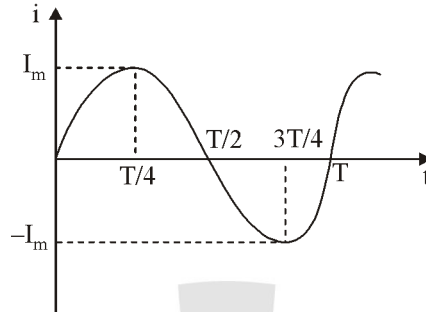
Magnetization force or magnetic field intensity (H)

$$H = \frac{NI}{l} \text{ ATs / m}$$



## 1.3 MAGNETIC HYSTERESIS CURVE

If ac current is made to flow through coil in the magnetic circuit shown above  $i = I_m \sin \omega t$



Time period

$$T = \frac{1}{f} = \frac{2\pi}{\omega}$$

Where

$$\omega = 2\pi f \text{ is frequency}$$

Let initially

$$B = 0$$

(i.e. residual magnetism is absent)

For  $0 < t < \frac{T}{4}$  where  $i$  increases from zero to  $I_m$  initially  $B$  increases linearly with  $H$  (or  $i$ ) and after a certain value of  $H$ ,  $B$  doesn't increase significantly i.e.  $B$  remains almost constant i.e. saturation.

For linear magnetic circuit

$$B \propto H$$

⇒

$$B = \mu H$$

⇒

$$B = \mu_0 \mu_r H$$

Where

$\mu$  = Permeability of iron core

$\mu_r$  = Relative permeability of core

$$\mu_0 = \text{Permeability free space} = 4\pi \times 10^{-7} \text{ H/m}$$

Flux linking

$$\phi = BA = \mu HA = \mu A \times \frac{Ni}{l} \quad (H = \frac{Ni}{l})$$

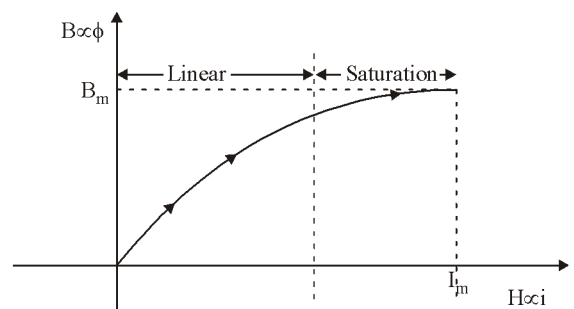
⇒

$$\phi = \frac{Ni}{l} = \frac{f}{Rl}$$

Where  $f = Ni$  (mmf in Amp-Turns) applied

$$Rl = \frac{l}{\mu A} \text{ reluctance of core}$$

mmf = Magneto-Motive Force

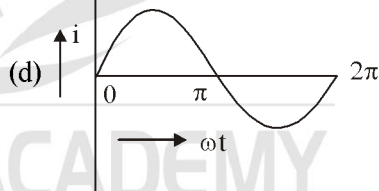
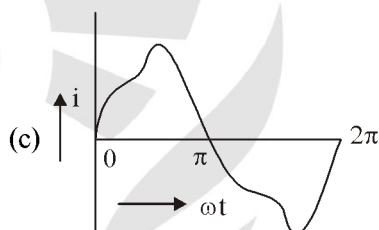
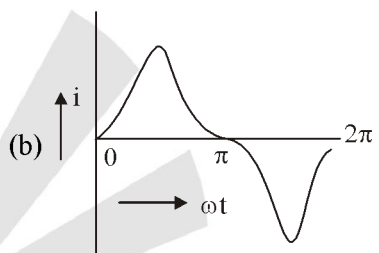
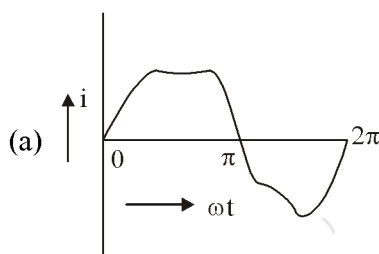


## PRACTICE SHEET

### OBJECTIVE QUESTIONS

1. Two transformers of the same type, using the same grade of iron and conductor materials, are designed to work at the same flux and current densities but the linear dimensions of one are two times those of the other in all respects. The ratio of kVA of the two transformers closely equals :  
 (a) 16                                      (b) 8  
 (c) 4                                        (d) 2
2. When a transformer winding suffers a short-circuit, the adjoining turns of the same winding experience:  
 (a) an attractive force (b) a repulsive force  
 (c) no force                                (d) none of the above
3. Supply to one terminal of a  $\Delta$ -Y connected three-phase core type transformer which is on no-load, fails. Assuming magnetic circuit symmetry, voltages on the secondary side will be (if supply voltage is 230 V):  
 (a) 230, 230, 115                      (b) 230, 115, 115  
 (c) 345, 115, 115                      (d) 345, 0, 345
4. Auto-transformer is used in transmission and distribution :  
 (a) when operator is not available  
 (b) when iron losses are to be reduced  
 (c) when efficiency considerations can be ignored  
 (d) when the transformation ratio is near to unity
5. Keeping in view the requirement of parallel operation, which of the 3-phase connections given below are possible?  
 (a) delta-delta to delta-star  
 (b) delta-delta to star-delta  
 (c) star-star to delta-star  
 (d) delta-star to star-delta
6. The laws of electromagnetic induction (Faraday's and Lenz's law) are summarized in the following equation  
 (a)  $e = iR$                                 (b)  $e = L \frac{di}{dt}$   
 (c)  $e = -\frac{d\psi}{dt}$                                 (d) none of these
7. The efficiency of a 100 kVA transformer is 0.98 at full as well as at half load. For this transformer at full load the copper loss.  
 (a) is less than core loss.  
 (b) is equal to core loss.  
 (c) is more than core loss  
 (d) none of the above
8. The magnetising current in a transformer is rich in :  
 (a) 3<sup>rd</sup> harmonic                          (b) 5<sup>th</sup> harmonic  
 (c) 7<sup>th</sup> harmonic                          (d) 13<sup>th</sup> harmonic
9. In a constant voltage transformer (CVT), the output voltage remains constant due to :  
 (a) capacitor                                (b) input inductor  
 (c) saturation                                (d) tapped windings
10. If an ac voltage wave is corrupted with an arbitrary number of harmonics, then the overall voltage waveform differs from its fundamental frequency component in terms of :  
 (a) only the peak values  
 (b) only the rms values  
 (c) only the average values  
 (d) all the three measures (peak, rms and average values)
11. A 220/440 V, 50 kVA single phase transformer operates on 220 V, 40 Hz supply with secondary winding. Then :  
 (a) the eddy current loss and hysteresis loss of the transformer decrease  
 (b) the eddy current loss and hysteresis loss of the transformer increase  
 (c) the hysteresis loss of the transformer increases while eddy current loss remains the same  
 (d) the hysteresis loss remains the same whereas eddy current loss decreases

12. The low voltage winding of a 400/230V, 1-phase, 50 Hz transformer is to be connected to a 25 Hz, the supply voltage should be :
- (a) 230 V                      (b) 460 V  
(c) 115 V                      (d) 65 V
13. A 50 Hz transformer having equal hysteresis and eddy current losses at rated excitation is operated at 45 Hz at 90% of its rated voltage. Compared to rated operating point the core losses under this condition :
- (a) reduce by 10%    (b) reduce by 19%  
(c) reduce by 14.5%    (d) remain unchanged
14. A 10 kVA, 400V/200V single phase transformer with 10% impedance draws a steady short circuit line current of :
- (a) 50A                      (b) 150A  
(c) 250A                      (d) 350A
15. A 400V/100V, 10 kVA two winding transformer is reconnected as an auto transformer across a suitable voltage source. The maximum rating of such an arrangement could be :
- (a) 50 kVA                      (b) 15 kVA  
(c) 12.5 kVA                      (d) 8.75 kVA
16. A 10 kVA, 400V/200V, single phase transformer with a percentage resistance of 3% and percentage reactance of 6% is supplying a current of 50A to a resistive load. The value of the load voltage is :
- (a) 194 V                      (b) 390 V  
(c) 192 V                      (d) 196 V
17. A 20-turn iron-cored inductor is connected to a 100V, 50Hz source. The maximum flux density in the core is  $1\text{Wb/m}^2$ . The cross-sectional area of the core is :
- (a)  $0.152\text{m}^2$                       (b)  $0.345\text{m}^2$   
(c)  $0.0225\text{m}^2$                       (d)  $0.56\text{m}^2$
18. A 220/220 volts, 50Hz transformer has a core flux density of  $1\text{Wb/m}^2$ , find its flux density in  $\text{Wb/m}^2$  when connected to 110 volts, 25Hz supply :
- (a) 0.25                      (b) 1.00  
(c) 4.00                      (d) zero
19. A single-phase transformer fed from a rated voltage supply operates at no-load. The core loss of the transformer is assumed to be negligible. The current drawn by the transformer from the supply will have the waveform.



20. The equivalent resistance and equivalent reactance of a transformer are respectively  $0.5\Omega$  and  $0.8\Omega$ . The voltage regulation will be zero when the load power factor is
- (a)  $\frac{0.8}{\sqrt{0.89}}$  lagging                      (b)  $\frac{0.5}{\sqrt{0.89}}$  lagging  
(c)  $\frac{0.5}{\sqrt{0.89}}$  leading                      (d)  $\frac{0.8}{\sqrt{0.89}}$  leading



31. In a transformer if primary leakage impedance is neglected, then
1. Magnetizing current lags the applied voltage  $V_1$  by  $90^\circ$
  2. Core loss current lags  $V_1$  by  $90^\circ$
  3. Exciting current lags  $V_1$  by  $90^\circ$
  4. Core loss current is in phase with  $V_1$
  5. Exciting current lags  $V_1$  by about  $80^\circ$
  6. Magnetizing current statements are from these the correct statement are
- (a) 1, 4, 5                      (b) 3, 4, 6  
(c) 1, 4                          (d) 1, 2, 6
32. A 50 Hz single phase transformer draws a short circuit current of 35A at 0.25 pf lag, when connected to 16V, 50 Hz source. What will be the pf if it is energized from 16V, 75 Hz source ?
- (a) 0.17 lagg.                      (b) 0.37 lagg.  
(c) 0.25 lagg.                      (d) 0.29 lagg.
33. When compared with power transformer, a distribution transformer has
- (a) Low percentage impedance and high  $I^2R$  loss to core loss ratio
  - (b) High percentage impedance and high  $I^2R$  loss to core loss ratio
  - (c) High percentage impedance and low  $I^2R$  loss to core loss ratio
  - (d) Low percentage impedance and low  $I^2R$  loss to core loss ratio
34. A transformer designed for operation of 60 Hz supply is worked on 50 Hz supply system without changing its voltage and current ratings. When compared with full load efficiency at 60 Hz, the transformer efficiency on full load at 50 Hz will be
- (a) Increase marginally
  - (b) Increase by a factor of 1.2
  - (c) remain unaltered
  - (d) decrease marginally
35. A bank of three identical single phase 250 kVA, 11 kV / 230 V transformer is used to provide 400V Low tension supply from a 11 kV, 3 phase substation the effective kVA rating of the bank will be
- (a) 250                              (b)  $250\sqrt{3}$   
(c) 500                                (d) 750
36. when a short circuit test is conducted on a single phase transformer, 30% of the rated voltage is required to allow full load current. The short circuit power factor is found to be 0.2 . The percentage regulation at u.p.f. is
- (a) 30                                  (b) 29.5  
(c) 15                                  (d) 6
37. An auto transformer has  $V_1, I_1$  as input quantities and  $V_2, I_2$  as output quantities with  $V_2 < V_1$  the VA conducted from input to output is
- (a)  $V_1 I_2$                               (b)  $V_2 I_1$   
(c)  $V_1 I_1 - V_2 I_2$                       (d)  $(V_1 - V_2) I_1$
38. A auto transformer has  $V_1, I_1$  as input quantities and  $V_2, I_2$  as output quantities with  $V_2 < V_1$  the VA transferred inductively from primary to secondary is
- (a)  $V_1 I_2$                               (b)  $V_2 I_1$   
(c)  $V_1 I_1 - V_2 I_2$                       (d)  $(V_1 - V_2) I_1$
39. A 400 V / 200 V transformer has a full load voltage regulation of x p.u. at 0.8 pf lagging if this transformer is used as on auto transformer with voltage rating 400 V / 600 V or 200 V / 600 V , then its voltage regulation would be
- (a)  $\frac{x}{3}, \frac{x}{3}$                                   (b)  $\frac{2x}{3}, \frac{x}{3}$   
(c)  $\frac{2x}{3}, \frac{2x}{3}$                                   (d)  $\frac{x}{3}, \frac{2x}{3}$